

# FV<sup>3</sup>: model configurations for NGGPS

S-J Lin and L. Harris

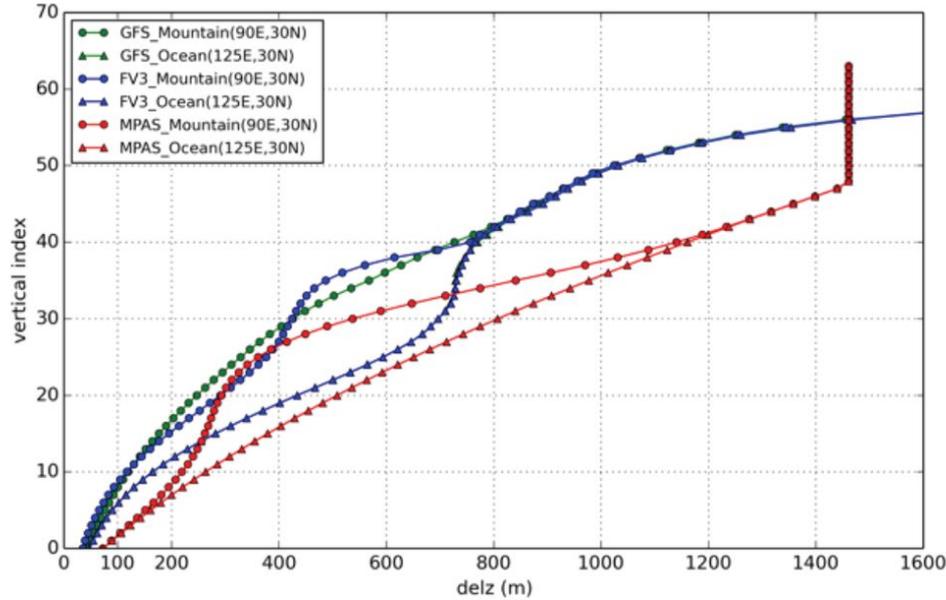
- Horizontal & vertical resolutions, physics & dynamics time steps
- FV<sup>3</sup>'s island-preserving terrain filter (same filtering philosophy as the FV transport scheme)
- Consistent parameters for model evaluations
- A note on the divergence & vorticity damping
- Two configurations for NGGPS:
  - 1) Implicit diffusion (monotonic constraints)
  - 2) Explicit diffusion and energy conservation

# FV<sup>3</sup> & MPAS configurations for NWP with GFS physics:

	Phase-1 MPAS	Phase-2 MPAS	C768 FV3	C640 FV3 (alt)	C1024 var 3	GFS_TL1534
Grid Type	Voronoi mesh	Voronoi mesh	Cubed-sphere	Cubed-sphere	Stretched-Cubed-sphere	Gaussian/Reduced-Gaussian
Total number of grid points	4,096,002	2,621,442	3,538,944	2,457,600	6,291,456	4,718,592/3,126,128
Avg. Resolution (km)	12	15	12.05	14.46	[3, 30]	13
Bottom layer thickness (m)	n/a	<b>72.5</b>	<b>28-50</b>	<b>28-50</b>	<b>28-50</b>	<b>28-50</b>
Short-wave rad time step (s)	n/a	<b>1800</b>	<b>3600</b>	<b>3600</b>	<b>3600</b>	<b>3600</b>
Long-wave rad time step(s)	n/a	<b>1800</b>	<b>3600</b>	<b>3600</b>	<b>3600</b>	<b>3600</b>
Phys time step(s)	n/a	<b>90</b>	<b>225</b>	<b>225</b>	<b>60</b>	<b>225</b>
Dynamic split steps	1	3	2	1	1	n/a
True dynamic time step (s)	72	30	112.5	225	60	450
Acoustic steps	6	6	6	10	12	n/a
Effective acoustic time step (s)	12	5	18.75	22.5	5	n/a

- From phase-1 to phase-2, MPAS total grid points reduced by 36% (12 km to 15 km)
- FV<sup>3</sup> *standard configuration* C768 (12.05 km) remains the same
- The *alternative configuration* FV<sup>3</sup> C640 (14.46 km) has 30% less grid points than C768
- FV<sup>3</sup> uses the same physics time step (225 sec) as GFS (per EMC instruction)
- MPAS uses a smaller 90 sec physics time step

# Vertical grids: GFS, FV3, and MPAS

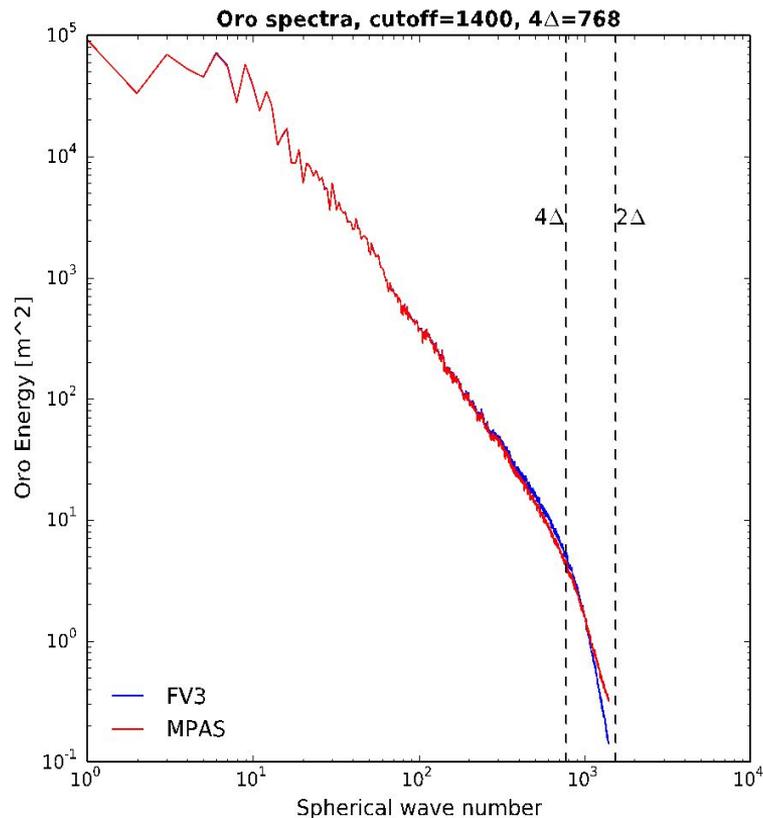


**Note: FV3 time step size is not limited by vertical CFL condition**

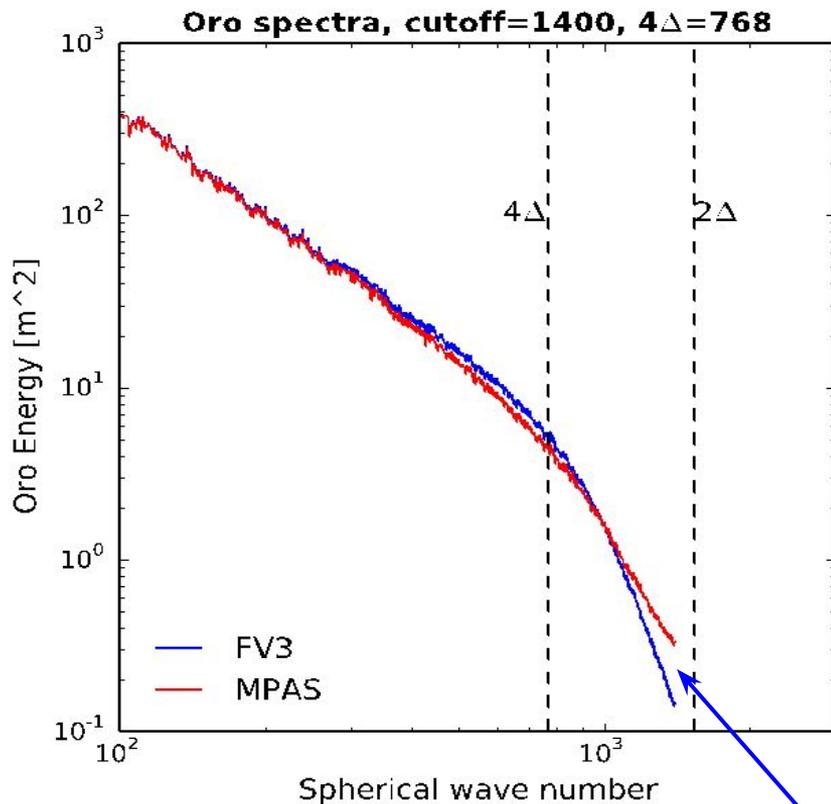
	<b>PBL &gt; 850 mb</b>	<b>Free Troposphere 850 - 150 mb</b>	<b>UTLS 150 - 50 mb</b>	<b>Upper stratosphere &lt; 50 mb</b>
<b>GFS</b>	<b>13</b>	<b>24</b>	<b>8</b>	<b>19</b>
<b>FV3</b>	<b>13</b>	<b>24</b>	<b>9</b>	<b>18</b>
<b>MPAS</b>	<b>9</b>	<b>24</b>	<b>6</b>	<b>25</b>

# FV3's island-preserving terrain filter

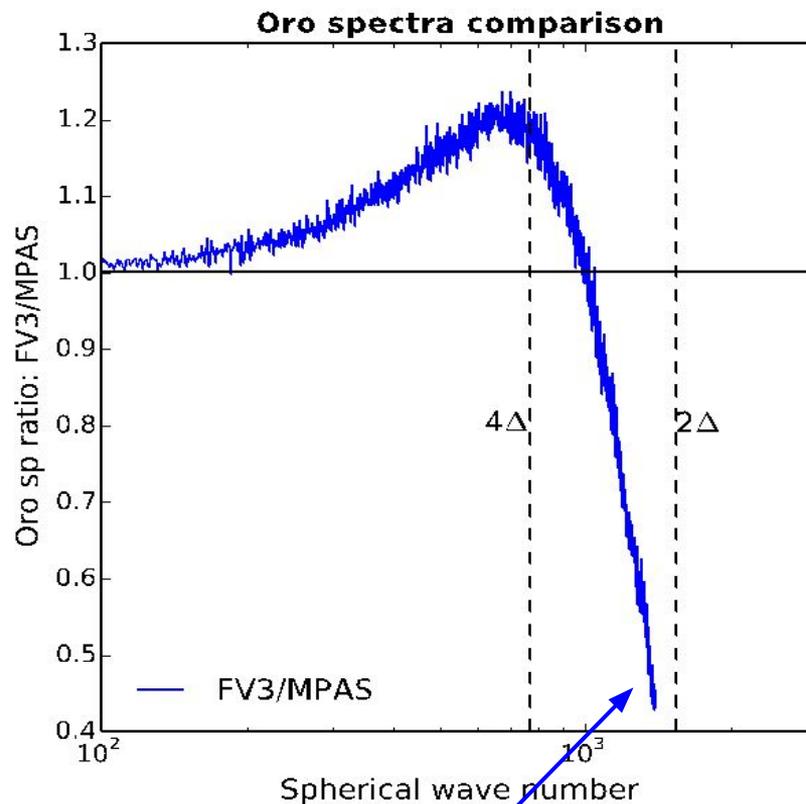
- Two passes of FCT filter for monotonicity, and preservation of land-sea mask.
  - 2-delta structures not supported by the dynamics are strongly suppressed.
- The FCT filter is the non-linear combination of del-4 and monotonic del-2 schemes



## The Orography spectra

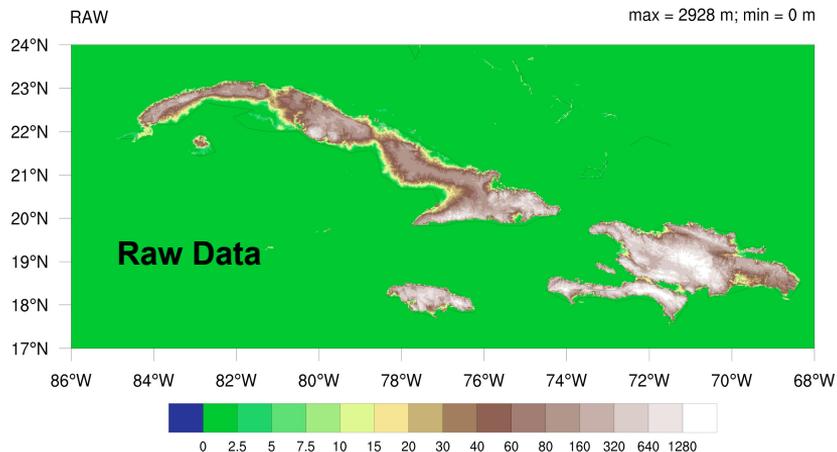
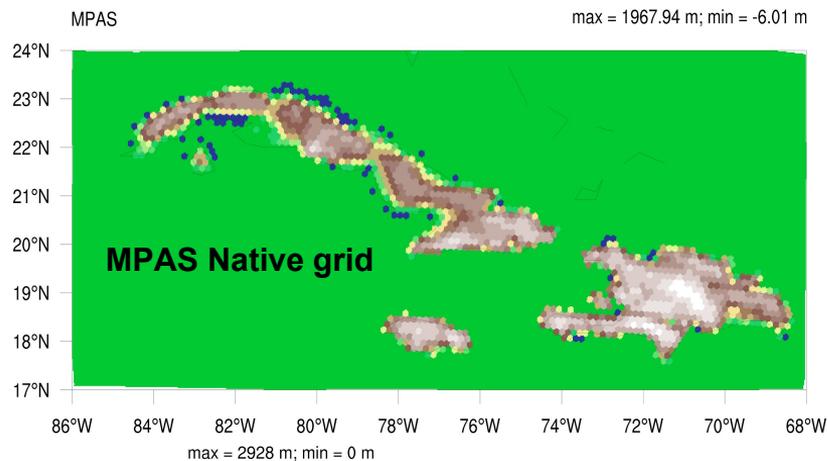
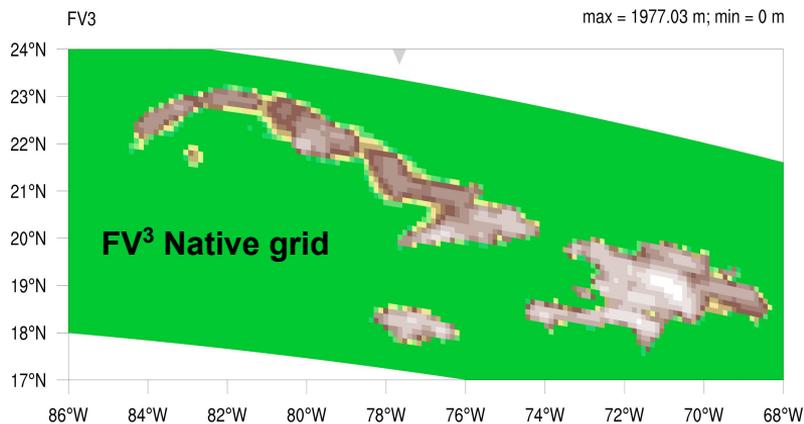


## The ratio: FV3/MPAS



**FV<sup>3</sup> applies more aggressive filter on 2-delta-waves**

# The island-preserving terrain filter of FV3 preserves well the peaks/valleys, and **does not produce negative mountains over ocean**



# Consistent parameters for model evaluations:

- Physics and dynamics should be tuned together as a package.
  - For NGGPS, the GFS physics should not be tuned
  - Only dynamical parameters (e.g., diffusion) can be tuned
- ***Unless the physics or model configuration is changed, one should never change any parameter from run to run.***
  - Parameters must be the same during the whole hindcast period or an AMIP run.
  - ***If one forecast fails, requiring a parameter change, one must re-make all the hindcast runs with the new parameters***
- Sensitivity tests, if needed, must be an open process, requiring iterations between the developers and the testers.

# Divergence & Vorticity damping:

- Vertical vorticity is transported by the FV algorithm. With monotonic advection there is no need to add explicit damping to the vorticity.
- Since the divergence is not damped implicitly, a scale-selective divergence damping (either del-4 or del-6) is used.
- The linear “5<sup>th</sup> order” scheme is FV<sup>3</sup>’s least diffusive scheme
  - Used at NASA/GMAO for 4D Var and at GFDL for ultra-high resolution (1-4 km) global cloud-resolving simulations.
- With the non-diffusive “linear” scheme, a scale-selective damping on vorticity and other fluxes is recommended. The lost KE can then be added locally as heat for better conservation of total energy

# FV<sup>3</sup> Namelist Document

Complete list of FV<sup>3</sup> namelist options  
has been sent to the DTG

Email S-J Lin or Lucas Harris if you  
would like another copy

Focusing on solver and diffusion options  
in this presentation; see document for  
complete coverage

# FV<sup>3</sup>

Namelist options in the GFDL  
Finite-Volume Cubed-Sphere Dynamical Core  
Shian-Jiann Lin and Lucas Harris  
Initial Version 12 Aug 2013  
Version 2.0a Revised 7 Jan 2016

## Entries in `fv_core_nml`

### Required options:

**layout** Integer(2): Processor layout on each tile. The number of PEs assigned to a domain must equal  $\text{layout}(1) * \text{layout}(2) * \text{ntiles}$ . Must be set.

**np<sub>x</sub>** Integer: Number of grid *corners* in the x-direction on one tile of the domain; so one more than the number of grid cells across a tile. On the cubed sphere this is *one more than* the number of cells across a cube face. Must be set.

**np<sub>y</sub>** Integer: Number of grid *corners* in the y-direction on one tile of the domain. This value should be identical to `npx` on a cubed-sphere grid; doubly periodic or nested grids do not have this restriction. Must be set.

**np<sub>z</sub>** Integer: Number of vertical levels. Each choice of `npz` comes with a pre-defined set of hybrid sigma-pressure levels and model top (see `atmos_cubed_sphere/tools/fv_eta.F90`). Must be set.

**ntiles** Integer: Number of tiles on the domain. For the cubed sphere, this should be 6, one tile for each face of the cubed sphere; normally for most other domains (including nested grids) this should be set to 1. Must be set.

### Initialization options:

**add\_noise** Real: amplitude of random thermal noise (in K) to add upon startup. Useful for perturbing initial conditions. -1 by default; disabled if 0 or negative.

# Domain specification

```
&fv_core_nml
```

```
npx = 769
```

```
npz = 64
```

```
npz = 64
```

```
n_sponge = 8
```

```
tau = 5.
```

```
rf_cutoff = 8.e2
```

```
d2_bg_k1 = 0.16
```

```
d2_bg_k2 = 0.02
```

```
hydrostatic = .F.
```

```
k_split = 2
```

```
n_split = 6
```

```
fv_sg_adj = 1800
```

```
nord = 1
```

```
d4_bg = 0.15
```

```
vtdm4 = 0.
```

```
do_vort_damp = .false.
```

```
d_con = 0.
```

```
hord_mt = 8
```

```
hord_vt = -8
```

```
hord_tm = -8
```

```
hord_dp = -8
```

```
hord_tr = -8
```

`npx` and `npz` control the number of grid corners across a cube face; subtract one to get the number of grid cells

`c768` corresponds roughly to  $\frac{1}{8}$  degree, or 12 km global average grid-cell width

`npz` is the number of grid levels, with a hard-coded specification of level placement

64-level model top at 0.28 mb

# Timestepping

```
&fv_core_nml
  npx   = 769
  npy   = 769
  npz   = 64
  n_sponge = 8
  tau   = 5.
  rf_cutoff = 8.e2
  d2_bg_k1 = 0.16
  d2_bg_k2 = 0.02
  hydrostatic = .F.
  k_split = 2
  n_split = 6
  fv_sg_adj = 1800
  nord = 1
  d4_bg = 0.15
  vtdm4 = 0.
  do_vort_damp = .false.
  d_con = 0.
  hord_mt = 8
  hord_vt = -8
  hord_tm = -8
  hord_dp = -8
  hord_tr = -8
```

```
&coupler_nml
  dt_atmos = 225
```

dt\_atmos is the physics timestep: **225 s**, matching GFS

Vertical remapping and advection is done k\_split times per physics timestep

**112.5 s**: Lagrangian vertical coordinate has *no* Courant number restriction!

Acoustic solver and horizontal dynamics called n\_split times between vertical remappings:

**18.75 s**: Forward-in-time solver

## Monotonic scheme

```
&fv_core_nml
  npx   = 769
  npy   = 769
  npz   = 64
  n_sponge = 8
  tau   = 5.
  rf_cutoff = 8.e2
  d2_bg_k1 = 0.16
  d2_bg_k2 = 0.02
  hydrostatic = .F.
  k_split = 2
  n_split = 6
  fv_sg_adj = 1800
  nord = 1
  d4_bg = 0.15
  vtdm4 = 0.
  do_vort_damp = .false.
  d_con = 0.
  hord_mt = 8
  hord_vt = -8
  hord_tm = -8
  hord_dp = -8
  hord_tr = -8
```

## Non-monotonic (“linear”) scheme

```
&fv_core_nml
  npx   = 769
  npy   = 769
  npz   = 63
  n_sponge = 8
  tau   = 5.
  rf_cutoff = 8.e2
  d2_bg_k1 = 0.16
  d2_bg_k2 = 0.02
  hydrostatic = .F.
  k_split = 2
  n_split = 6
  fv_sg_adj = 1800
  nord = 1
  d4_bg = 0.15
  vtdm4 = 0.04
  do_vort_damp = .true.
  d_con = 1.
  hord_mt = 6
  hord_vt = -5
  hord_tm = -5
  hord_dp = -5
  hord_tr = -8
```

Optimized monotonic and non-monotonic (“linear”) schemes for computing fluxes. Tracer advection is *always* monotonic (-8) and is *never* explicitly diffused

**Monotonic scheme (+8, -8)** is intrinsically diffusive to 2-delta-waves. Explicit horizontal damping from 4th-order (nord = 1) divergence damping

No explicit (“vorticity”) damping on other fluxes

```
do_vort_damp = .false.
```

## Monotonic scheme

```
&fv_core_nml
  npx   = 769
  npy   = 769
  npz   = 64
  n_sponge = 8
  tau   = 5.
  rf_cutoff = 8.e2
  d2_bg_k1 = 0.16
  d2_bg_k2 = 0.02
  hydrostatic = .F.
  k_split = 2
  n_split = 6
  fv_sg_adj = 1800
  nord = 1
  d4_bg = 0.15
  vtdm4 = 0.
  do_vort_damp = .false.
  d_con = 0.
  hord_mt = 8
  hord_vt = -8
  hord_tm = -8
  hord_dp = -8
  hord_tr = -8
```

## Non-monotonic ("linear") scheme

```
&fv_core_nml
  npx   = 769
  npy   = 769
  npz   = 64
  n_sponge = 8
  tau   = 5.
  rf_cutoff = 8.e2
  d2_bg_k1 = 0.16
  d2_bg_k2 = 0.02
  hydrostatic = .F.
  k_split = 2
  n_split = 6
  fv_sg_adj = 1800
  nord = 1
  d4_bg = 0.15
  vtdm4 = 0.04
  do_vort_damp = .true.
  d_con = 1.
  hord_mt = 6
  hord_vt = -5
  hord_tm = -5
  hord_dp = -5
  hord_tr = -8
```

**Non-monotonic scheme (6, -5)**  
applies *no* monotonicity constraint  
("linear"), only a 2dx filter to suppress  
oscillations.

Needs consistent damping to vorticity  
and momentum fluxes. This damping  
(vtdm4) should be weaker than the  
divergence damping.

The local dissipated kinetic energy is  
added back as heat ( $d\_con > 0$ )

# The 2-dz filter

```
&fv_core_nml
  npx   = 769
  npy   = 769
  npz   = 64
  n_sponge = 8
  tau   = 5.
  rf_cutoff = 8.e2
  d2_bg_k1 = 0.16
  d2_bg_k2 = 0.02
  hydrostatic = .F.
  k_split  = 2
  n_split  = 6
  fv_sg_adj = 1800
  nord    = 1
  d4_bg   = 0.15
  vtdm4   = 0.
  do_vort_damp = .false.
  d_con   = 0.
  hord_mt = 8
  hord_vt = -8
  hord_tm = -8
  hord_dp = -8
  hord_tr = -8
```

The 2-dz filter is a *local* vertical mixing to suppress K-H instabilities on the relaxation timescale `fv_sg_adj`, using ideas similar to those of Smagorinsky and Lilly.

Here, it is applied only on the top `n_sponge` levels to suppress instability due to the accumulation of vertically-propagating waves at the model top

The filter conserves energy, air and tracer mass, and momentum.

This is the *only* explicit vertical diffusion in FV<sup>3</sup>, and is not strictly necessary; used as a safety valve to ensure model stability under adverse conditions

# Rayleigh damping and sponge layer

```
&fv_core_nml
  npx   = 769
  npy   = 769
  npz   = 64
  n_sponge = 8
  tau = 5.
  rf_cutoff = 8.e2
  d2_bg_k1 = 0.16
  d2_bg_k2 = 0.02
  hydrostatic = .F.
  k_split = 2
  n_split = 6
  fv_sg_adj = 1800
  nord = 1
  d4_bg = 0.15
  vtdm4 = 0.
  do_vort_damp = .false.
  d_con = 0.
  hord_mt = 8
  hord_vt = -8
  hord_tm = -8
  hord_dp = -8
  hord_tr = -8
```

Rayleigh damping is applied *consistently* to (u, v, w), converting lost kinetic energy to heat, with the same timescale (5 days) as in GFS

Rayleigh damping is only applied above `rf_cutoff` (in Pa); the top 6 layers in this case

Sponge layer is active in the top two layers of the model, using second-order horizontal damping to suppress wave-reflection